



# Miniaturized Dual Bandstop Filter using CRLH Transmission Line

Samar Refaat  
Benha Faculty of Engineering  
Benha University  
Benha ,Egypt

Amr A. Al-Awamry  
Benha Faculty of Engineering  
Benha University  
Benha,Egypt

A. A. Mitkees  
MTC  
Cairo ,Egypt

## ABSTRACT

Design of a dual wide bandstop filter is proposed based on Composite Right and Left-Handed Transmission-line (CRLH-TL) . Two stop bands with center frequencies of 8.3 GHz and 12.9 GHz are achieved with fractional bandwidths 57.8% and 32.5% respectively. Spiral interdigital capacitors and stub inductors are employed to designed filter. The proposed bandstop filter provides low passband insertion loss, better attenuation in stopbands, and low cost. The total filter size is about 7.8mm×15.1mm which is very compact compared to other metamaterial and conventional microstrip filters. Filter is also fabricated and measured to demonstrate the performance matched with simulation results.

## Keywords

Composite Right and Left-Handed Transmission-line (CRLH-TL), Dual band filter, Metamaterials, Spiral interdigital capacitor, Stub inductors.

## 1. INTRODUCTION

Bandstop filters are essential building blocks in wireless systems. They play an important role of filtering out unwanted signals. Compact design, high rejection in stopbands, and high selectivity are important characteristics of bandstop filters. There are different methods to design these filters, it is designed by using quarter-wavelength short-circuited stubs[11], another bandstop filters using stepped-impedance open-circuited stubs are designed in papers [5]-[6]-[8]-[10]- [12] but large size and narrow stopband are problems of these designed filters.

In [14], a dual bandstop filter is achieved by using three-section stepped impedance resonators (SIRs), or a dual-mode loop resonator [15]. A compact dual band BSFs may also be realized by combining a spur-line structure and a rectangle slot [16]. Dual band BSF composed of meandered slot defected microstrip structure and simplified spiral microstrip resonator is developed in [17] to obtain independently controlled stopbands and improved spurious response. Another methods and structures have been proposed [18-21]. In [18] ,two square SRRs are placed on the same transverse plane realizing two independent reject bands.

A compact dual band bandstop filter with sharp rejection using transversal signal interaction, consisting of a transmission line path and a cascaded coupled line path, is proposed [19]. In [20],dual and tri band bandstop filters are designed using I-stubs embedded within a meandered defected microstrip structure. Also, a dual band bandstop filter is based on open stubs and two equivalent T-shaped lines [21].

Early in 1968, Veselago first introduced the concept of left-handed material (LHM) with negative permittivity and

negative permeability [13]. In his paper, Veselago speculated on the possible existence of LHMs and anticipated their unique electromagnetic properties. First artificial LHM composed of thin wire cylinder and split-ring resonators (SRR) was realized by researchers such as Pendry et al. [9]Smith et al.[7]. SRR-based LHM only exhibit LH properties around the resonance of SRR. Therefore, realization of LHM using SRRs is not practical for microwave engineering applications as narrow-band and lossy due to requirement of operation near SRR resonance. To overcome drawbacks of SRR-based LHM, several researchers [1]-[4] soon realized that a transmission line can be used to realize a non-resonant LHM. LH transmission line approach is based on dual configuration of a RH/conventional transmission line, a composite right/left handed transmission line (CRLH-TL) structure provides left-handed (LH) and right-handed (RH) characteristics was first proposed by Caloz and Itoh [2]. New miniaturized antennas and microwave components/devices can be created for wireless communications and defense industries using LHM .

In this paper, A dual compact composite right/left handed transmission line (CRLH-TL) bandstop filter is designed. CRLH-TL structure is implemented in the form of spiral interdigital capacitors and stub inductors and our novel dual stop band filter has two stop bands with center frequencies of 8.3GHz and 12.9GHz and fractional bandwidth (FBW) 57.8% and 32.5% ,respectively. Total filter size is about 7.8mm×15.1mm.

The remaining content of this paper is organized as follows. In section 2 ,equivalent circuit model of a CRLH transmission line structure and its theory. In Section 3, design of proposed filter. In section 4, simulation and measurement results of fabricated filter. Finally, conclusion of this work is presented in section 5.

## 2. EQUIVALENT CIRCUIT MODEL OF A CRLH TRANSMISSION LINE STRUCTURE AND ITS THEORY

Left-handed materials(LHMs), are referred as metamaterials, which have simultaneously negative permittivity( $\epsilon$ ) and negative permeability ( $\mu$ )[13]. LHMs are dual of right-handed materials (RHMs) / conventional materials, a pure LH transmission line doesnot exist alone without RH transmission line because of RH parasitic effects, so combination of LH and RH structure form a composite right/left handed (CRLH) transmission line. Equivalent circuit model of Symmetric CRLH unit structure is shown in Fig.1 ,and propagation constant for a lossless CRLH transmission line is given by[3]

$$\beta_{\text{CRLH}} = s(\omega) \sqrt{\omega^2 L_R C_R + \frac{1}{\omega^2 L_L C_L} - \left( \frac{L_R}{L_L} + \frac{C_R}{C_L} \right)} \quad (1)$$

where:

$$s(\omega) = \begin{cases} -1 & \text{if } \omega < \omega_{\Gamma 1} = \min(\omega_{se}, \omega_{sh}) \\ +1 & \text{if } \omega > \omega_{\Gamma 2} = \max(\omega_{se}, \omega_{sh}) \end{cases} \quad (2)$$

,and

$$\omega_{se} = \frac{1}{\sqrt{L_R C_L}} \quad (3)$$

$$\omega_{sh} = \frac{1}{\sqrt{L_L C_R}} \quad (4)$$

$\omega_{se}$ ,  $\omega_{sh}$  are series and shunt resonances of CRLH series and shunt branches respectively. A dispersion diagram for a CRLH unit-cell is shown in Fig. 2. When  $\omega_{se}$  and  $\omega_{sh}$  are not equal, stop-band is generated between transition from LH to RH propagation (unbalanced case). In balanced case,  $\omega_{se} = \omega_{sh}$  and no stop-band between transition from LH to RH. Right and Left handed cutoff frequencies  $\omega_{CR}$ ,  $\omega_{CL}$  respectively are given by[3]

$$(\omega_{CR})_{\text{balanced}} = \frac{2}{\sqrt{L_R C_R}} \quad (5)$$

$$(\omega_{CL})_{\text{balanced}} = \frac{1}{2\sqrt{L_L C_L}} \quad (6)$$

$$(\omega_{CR})_{\text{unbalanced}} = \sqrt{\frac{[k+(2/\omega_L)^2]\omega_0^2 + \sqrt{[k+(2/\omega_L)^2]^2 \omega_0^4 - 4}}{2}} \quad (7)$$

$$(\omega_{CL})_{\text{unbalanced}} = \sqrt{\frac{[k+(2/\omega_L)^2]\omega_0^2 - \sqrt{[k+(2/\omega_L)^2]^2 \omega_0^4 - 4}}{2}} \quad (8)$$

where:

$$k = L_R C_L + L_L C_R \quad (9)$$

,and

$$\omega_R = \frac{1}{\sqrt{L_R C_R}} \quad (10)$$

$$\omega_L = \frac{1}{\sqrt{L_L C_L}} \quad (11)$$

A CRLH TL structure has a band-pass when  $\omega_{CL} < \omega_{CR}$  and has a band-stop characteristic when  $\omega_{CL} > \omega_{CR}$ . The centre frequency of band-pass or band-stop can be given by

$$\omega_0 = \sqrt{\omega_{se} \omega_{sh}} = \frac{1}{\sqrt[4]{L_R C_R L_L C_L}} \quad (12)$$

and a characteristic impedance ( $z_0$ ) of balanced and unbalanced CRLH are given by (13-14) respectively,

$$(z_0)_{\text{balanced}} = \sqrt{\frac{L_L}{C_L}} = \sqrt{\frac{L_R}{C_R}} \quad (13)$$

$$(z_0)_{\text{unbalanced}} = \sqrt{\frac{Z}{Y}} \quad (14)$$

where:

Z and Y are a series branch impedance and a shunt branch admittance in a CRLH unit cell, respectively.

Above equations are used to get L and C parameters when cutoff frequencies are known or used to get cutoff frequencies when circuit parameters are given.

### 3. DESIGN OF PROPOSED DUAL BANDSTOP FILTER

A microstrip implementation of a CRLH-TL composed of interdigital capacitance and shorted stub inductance is proposed here. Structure of proposed dual bandstop filter is shown in Fig. 3. It is represented by a symmetric unbalanced CRLH-TL unit cell ( $\omega_{se} \neq \omega_{sh}$ ), so filter has two bands. Proposed filter consists of two spiral interdigital capacitor represented  $C_L$  and shorted stub between them represented  $L_L$  in a symmetric CRLH-TL unit (fig.1). Spiral interdigital capacitor is used to realize miniaturization compared to original interdigital capacitor, also Shorted stub is bent as a meander line coil to reduce total size. So, the filter is less size than other conventional bandstop filters.

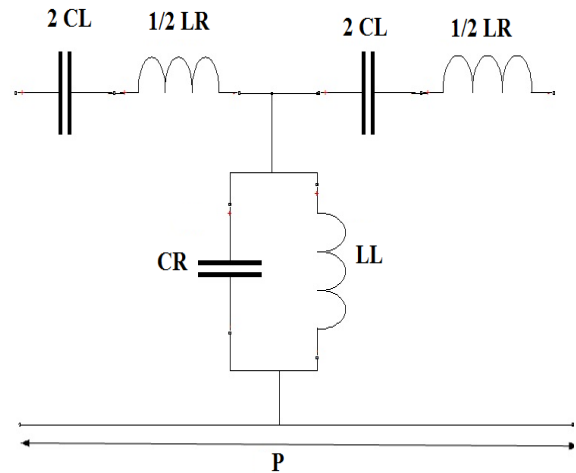


Fig. 1: Equivalent circuit of symmetric unit cell of a CRLH TL

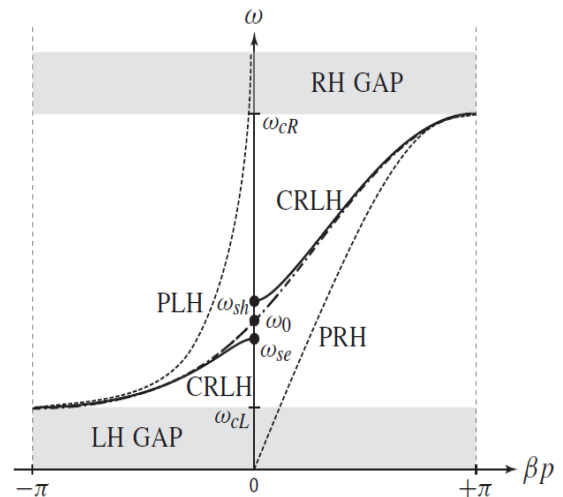


Fig. 2: A dispersion diagram for a CRLH unit-cell

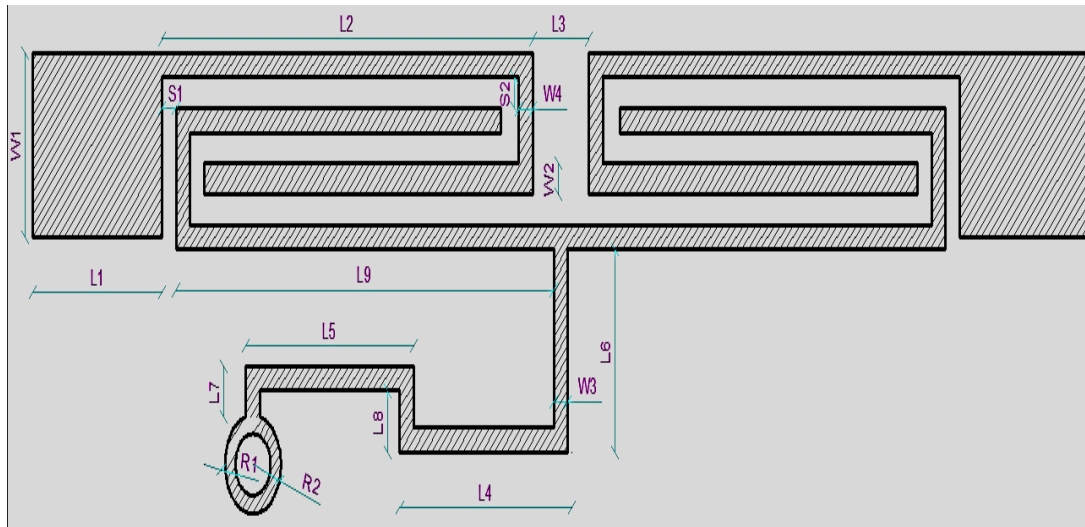


Fig 3: The structure of dual band BSF

#### 4. SIMULATION AND MEASUREMENT RESULTS OF THE FILTER

A dual proposed bandstop filter is constructed on substrate Rogers 5880 ( $\epsilon_r=2.2$  and  $h=0.508$  mm) with size  $7.8\text{mm} \times 15.1\text{mm}$  and dimensions of proposed filter are :

$W1=1.5\text{mm}$ ,  $L1=1.85\text{mm}$ ,  $L2=5.3\text{mm}$ ,  $W2=0.25\text{mm}$ ,  
 $S1=0.2\text{mm}$ ,  $S2=0.25\text{mm}$ ,  $W3=0.2\text{mm}$ ,  $L3=0.8\text{mm}$ ,  
 $W4=0.2\text{mm}$ ,  $L4=2.4\text{mm}$ ,  $L5=2.2\text{mm}$ ,  $R1$ (radius of  
 via)= $0.25\text{mm}$ ,  $R2=0.4\text{mm}$ ,  $L6=1.65\text{mm}$ ,  $L7=0.4\text{mm}$ ,  
 $L8=0.5\text{mm}$ ,  $L9=5.4\text{mm}$ . Filter is simulated with Ansoft HFSS with  $50 \Omega$  matching impedance.

Fabricated filter with attached SMA connectors is photographed in Fig. 4 and it is measured using a Vector Network Analyzer. Fig. 5 shows simulated and measured results of the filter. Simulated results show that two stop bands with center frequencies of 8.3 GHz and 12.9 GHz are achieved with fractional bandwidths 57.8% and 32.5% respectively ( first stopband from 5.9GHz to 10.7GHz and second stopband from 10.8 GHz to 15 GHz ), there is small difference between measured and simulated data as second stopband in measured results is shifted 150 MHz due to manufacturing possibilities . Insertion loss is less than 1dB in upper and lower passbands, minimum simulated and measured attenuation at first stopband are 68dB and 65dB respectively, and at second stopband are 40dB and 44dB respectively.

The simulated group delay is less than 0.5 ns which is depicted in Fig. 6 and Fig. 7 shows the phase scattering parameters for S11 and S21 responses within the swept frequency range from 4 to 18 GHz and within output phase angle range from  $-200$  to  $200$  degrees. These responses include some frequency jumps which are the significant properties of elliptic filters. Accordingly, the intersection between S11 and S21 responses can be recognized easily, especially nearby resonant frequency. Filter has advantage of a compact size of  $7.8\text{mm} \times 15.1\text{mm}$ . Finally, comparison of results for several reported dual band BSFs [14-21] is shown in Table 1.

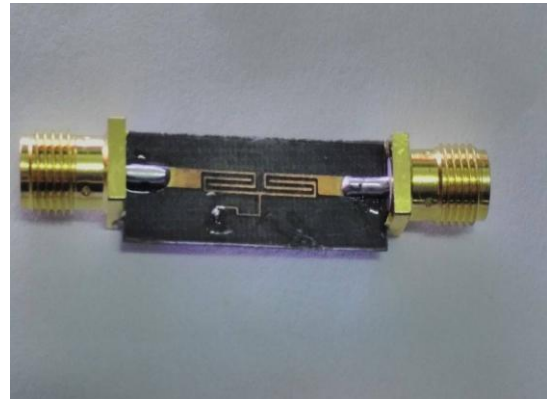


Fig. 4: Fabricated filter photograph

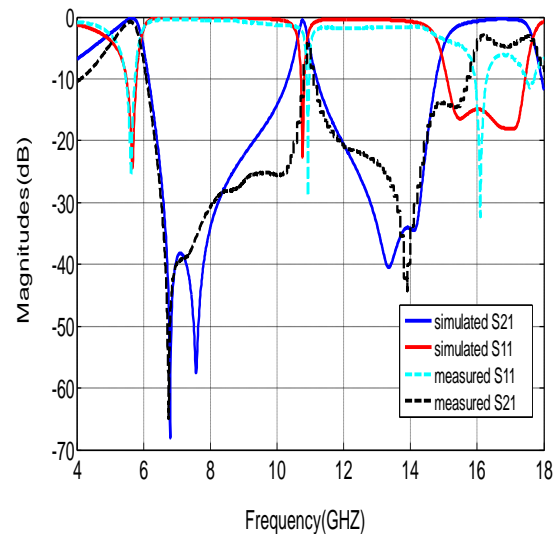


Fig .5: Simulated and measured results of a fabricated filter

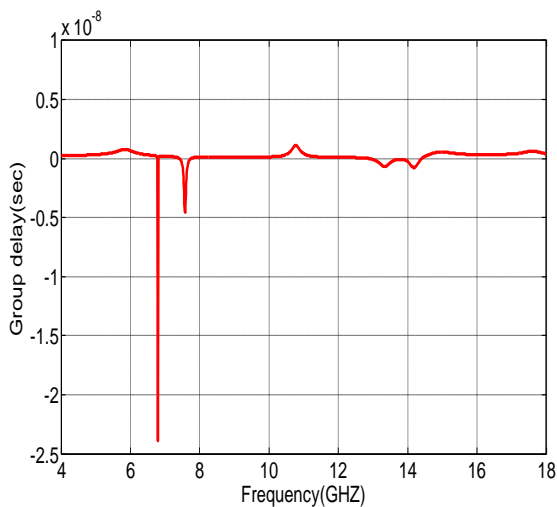


Fig. 6: Simulated group delay of proposed dual BSF

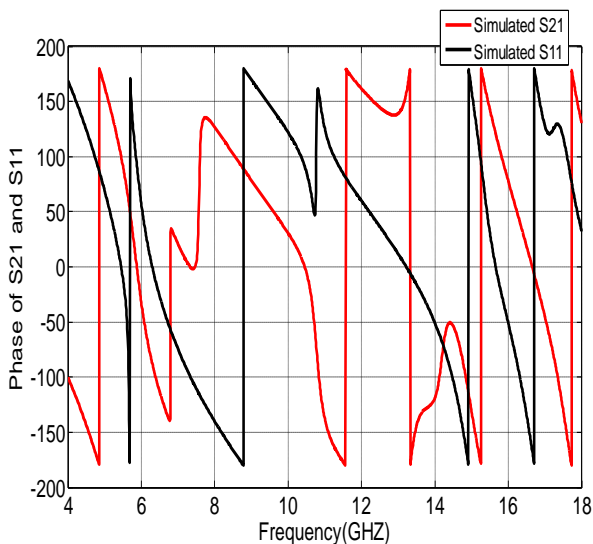


Fig. 7: The Phase responses of proposed dual BSF

Table 1. Comparison with the reported dual band BSFs.

Ref.	First Stopband Freq (GHz) / Rej (dB)	Second Stopband Freq (GHz) / Rej (dB)	Passband Performance
[14]	1.5/39.8	3.11/42	Normal
[15]	2.1/37	6.40/30	Normal
[16]	2.12/19.4	2.9/22.1	Normal
[17]	2.37/31.4	3.54/36.7	Good
[18]	9.8/25	11.35/25	Normal
[19]	2.4/44	3.7/34	Good
[20]	2.52/30.5	6.78/29.2	Normal
[21]	2.0/35	3.0/27	Normal
This Work	8.3/30.2	12.9/40	Good

(Freq. and Rej. represent the center frequency and rejection level of the stopband correspondingly. Passband performance denotes the insertion losses and return losses of lower/middle/upper passbands).

## 5. CONCLUSION

A miniaturized wide dual band bandstop filter based on unbalanced composite right/left-handed transmission line has been proposed. The presented dual band bandstop filter is designed using spiral interdigital capacitors and stub inductors. Two stop bands with center frequencies of 8.3 GHz and 12.9 GHz are achieved with fractional bandwidths 57.8% and 32.5%, respectively. The filter is designed, fabricated and measured. Results show agreement between simulation and measurement. The filter is low cost, very compact in size (7.8mm×15.1mm) and suitable for microwave communication systems. Multiband filters using CRLH-TLs and its modified models will be discussed in the future as multiband filters are important for different wireless and RFID applications.

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